

# **First conclusions of PCM viscosity measurements in the frame of Task 42- Annex 29-IEA**

**1<sup>st</sup> PCM Rheometry Workshop, FREIBURG, 7<sup>th</sup> March 2018**



# Introduction

## Contributors and equipments

| Institution                | Instrument            | Method                                 | Geometries                          | T controller                | T controlled-hood/<br>heated geometry | Min T (rot)<br>[ $\mu\text{N}\cdot\text{m}$ ] | Min T (osc)<br>[ $\mu\text{N}\cdot\text{m}$ ] |
|----------------------------|-----------------------|----------------------------------------|-------------------------------------|-----------------------------|---------------------------------------|-----------------------------------------------|-----------------------------------------------|
| Fraunhofer ISE             | MCR 502, Anton Paar   | Controlled stress rheometer            | Plate 60 mm                         | Peltier plate               | Yes                                   | 0.001                                         | 0.0005                                        |
|                            |                       |                                        | Concentric cylinder                 | Peltier concentric cylinder | Yes                                   |                                               |                                               |
| University of Zaragoza-I3A | AR-G2, TA Instruments | Controlled stress rheometer            | Plate 40 mm made of stainless steel | Peltier plate               | No                                    | 0.01                                          | 0.003                                         |
| University of Bayreuth     | Imeter, Method 5 DiVA | Translational viscometer and rheometer | Concentric cylinder                 | Temperature chamber         |                                       |                                               |                                               |

## Materials

| Product                    | Supplier           | T <sub>m</sub> (°C) |
|----------------------------|--------------------|---------------------|
| Parafol 18-97 (Octadecane) | Sasol              | 28°C                |
| RT70 HC                    | Rubitherm          | 70°C                |
| Standard oil S3            | Paragon Scientific | -                   |

# 2

## Methodology

**Starting point** → *Determining the rheological behavior of octadecane as phase change material.*

Thermochimica Acta 548 (2012) pp. 81-87.

## Procedure in rotational mode:

### 1. Conditioning step

- Without shear rate during 5 minutes at 25°C, to guarantee the set temperature

### 2. Steady state flow

- In logarithm mode from 0,001 to 1000 s<sup>-1</sup>, measuring 10 points per decade.
- Conditions of steady flow: Tolerance lower than 5%, during three consecutive measurements. Maximum time if tolerance is not fulfilled=1 minute

**10 seconds to measure the displacement by the optical encoder!!**

### Procedure in oscillatory mode:

#### 1. Conditioning step

Without shear rate during 5 minutes at 25°C, to guarantee the set temperature

#### 2. Stress sweep step

In logarithm mode from 0,01 to 100 Pa at a frequency of 1 Hz at 25°C, measuring 10 points per decade.

#### 3. Conditioning step

Without shear rate during 5 minutes at 25°C, to guarantee the set temperature

#### 4. Frequency sweep step

In logarithm mode from 0,01 to 100 Hz at a stress within the linear viscoelastic region (determined by 2, a stress value when  $G'$  is constant) at 25°C, measuring 10 points per decade.



- A sample with a gap around 0.5 and 1 mm should be tested in the case of using a plate geometry.
- **Temperature ramp in rotational mode:**

Conditioning step: Without shear rate during 20 minutes at 45°C, to guarantee the set temperature.

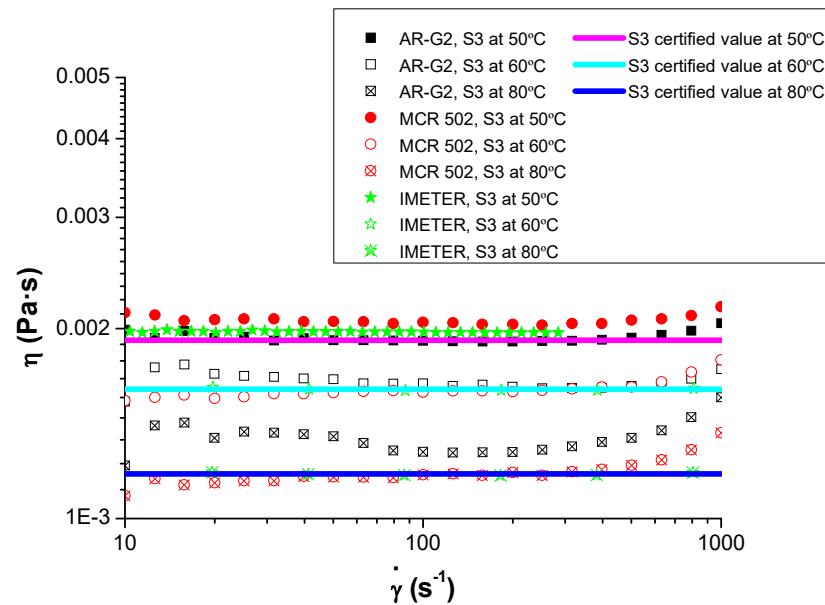
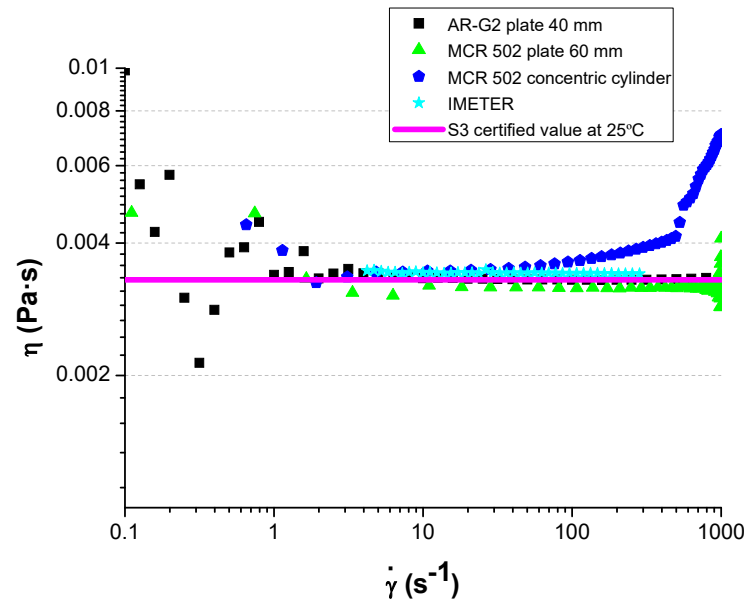
Temperature ramp: At 100 s<sup>-1</sup>(shear within the defined experimental window) from 45 to 25°C at a cooling rate of 0.5 K/min.
- **Temperature ramp in oscillatory mode:**

Conditioning step: Without shear rate during 20 minutes at 45°C, to guarantee the set temperature.

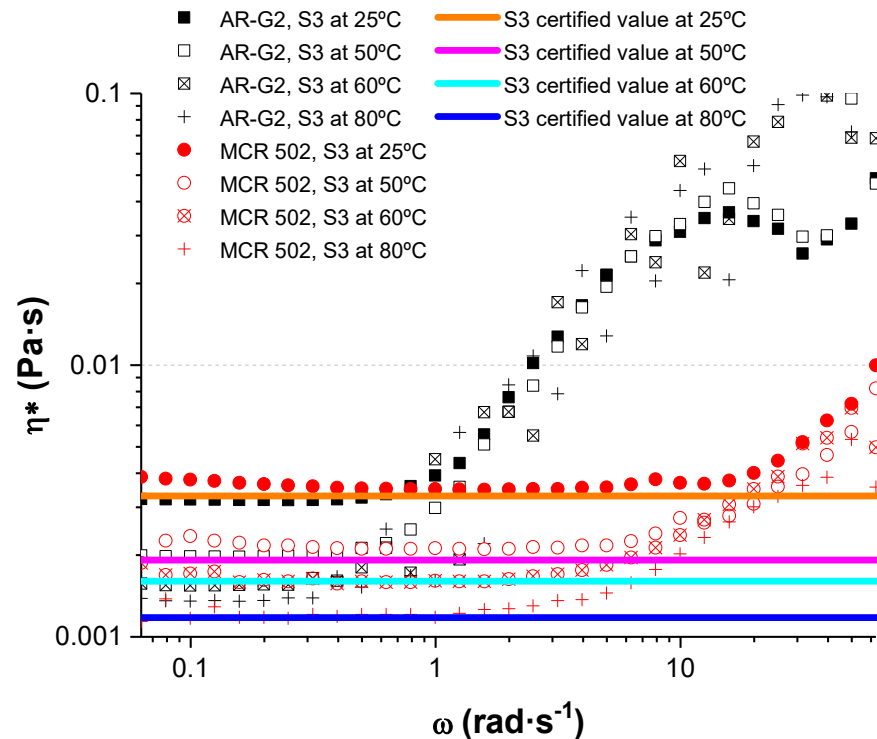
Temperature ramp: At 1 Hz (frequency within the defined experimental window) and with a stress of 1 Pa from 45 to 25°C at a cooling rate of 0.5 K/min.

# 3

## Results



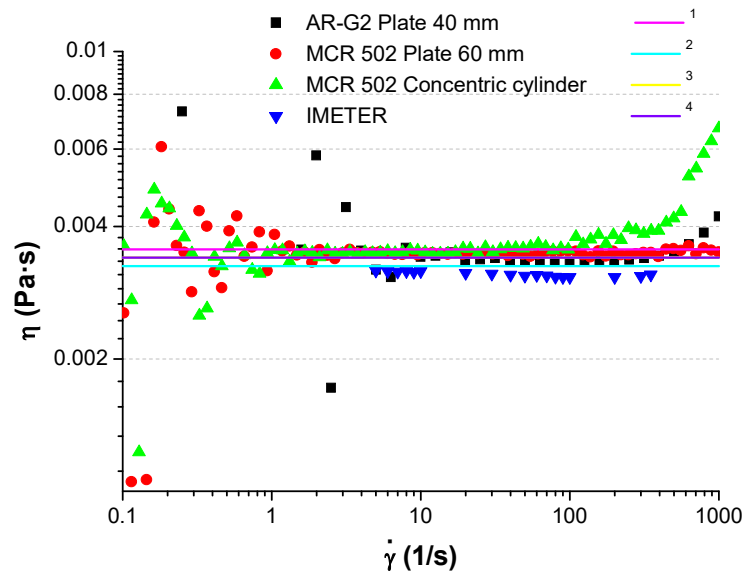
|             | Shear rate range<br>(s <sup>-1</sup> ) | Average<br>deviation<br>(%) | Relative standard<br>uncertainty (%) |
|-------------|----------------------------------------|-----------------------------|--------------------------------------|
| <b>25°C</b> |                                        |                             |                                      |
| AR-G2       | 2-1000                                 | 1.00                        | 0.26                                 |
| MCR 502     | 1.65-982                               | -3.77                       | 0.34                                 |
| IMETER      | 4.22-283.10                            | 2.03                        | 0.08                                 |
| <b>50°C</b> |                                        |                             |                                      |
| AR-G2       | 6.31-1000                              | 1.20                        | 0.39                                 |
| MCR 502     | 12.60-794                              | 7.18                        | 0.24                                 |
| IMETER      | 7.13-284.18                            | 1.33                        | 0.06                                 |
| <b>60°C</b> |                                        |                             |                                      |
| AR-G2       | 10-1000                                | 3.12                        | 0.66                                 |
| MCR 502     | 5.01-794                               | -0.92                       | 0.50                                 |
| IMETER      | 2.10-808.70                            | 0.85                        | 0.54                                 |
| <b>80°C</b> |                                        |                             |                                      |
| AR-G2       | 79.43-251.20                           | 8.05                        | 0.17                                 |
| MCR 502     | 5.01-794                               | -1.10                       | 0.75                                 |
| IMETER      | 2.10-803.6                             | 1.43                        | 0.87                                 |



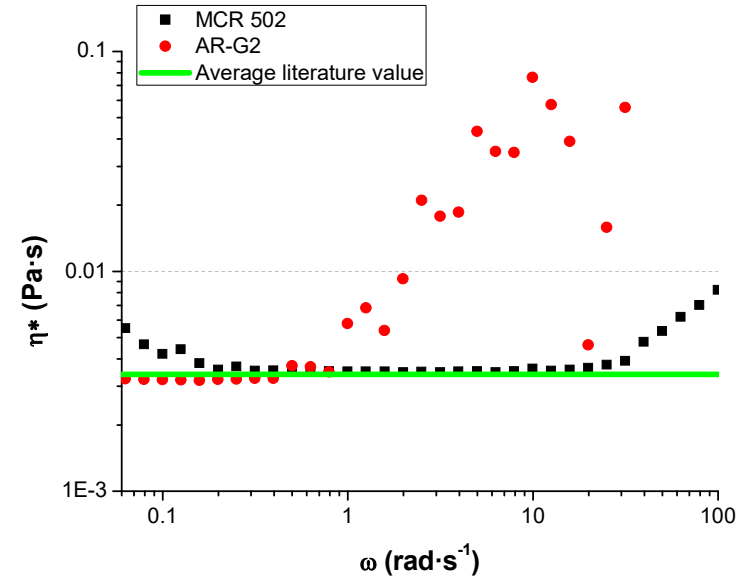
|         | Shear rate range (s <sup>-1</sup> ) | Average deviation (%) | Relative standard uncertainty (%) |
|---------|-------------------------------------|-----------------------|-----------------------------------|
| 25°C    |                                     |                       |                                   |
| AR-G2   | 0.06-0.79                           | -1.59                 | 1.04                              |
| MCR 502 | 0.25-4.99                           | 6.73                  | 0.28                              |
| 50°C    |                                     |                       |                                   |
| AR-G2   | 0.06-0.40                           | 3.86                  | 0.42                              |
| MCR 502 | 1.58*                               | 9.54                  | -                                 |
| 60°C    |                                     |                       |                                   |
| AR-G2   | 0.06-0.40                           | -1.80                 | 0.76                              |
| MCR 502 | 0.08-3.15                           | 2.02                  | 0.75                              |
| 80°C    |                                     |                       |                                   |
| AR-G2   | Deviation higher than 10%           |                       |                                   |
| MCR 502 | 0.10-1.99                           | 2.60                  | 0.84                              |

- An experimental window with limits must be established to avoid inappropriate results at low shear rates because the low torque and at high shear rates due to instrument and sample inertia.
- All the instruments obtain precise and accurate results within those shear rate ranges with the exception of the AR-G2 at 80°C, due to temperature gradients inside the sample, since the geometry used was not an upper heated plate for Peltier plate

## Rotational mode

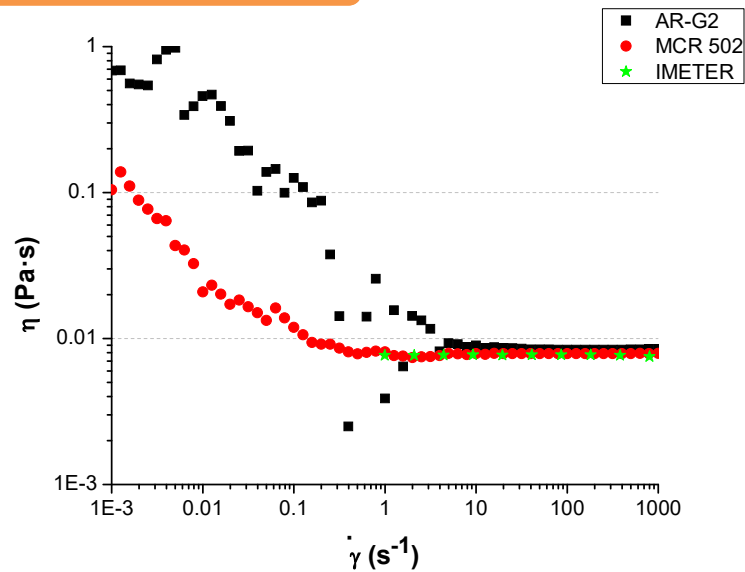


## Oscillatory mode

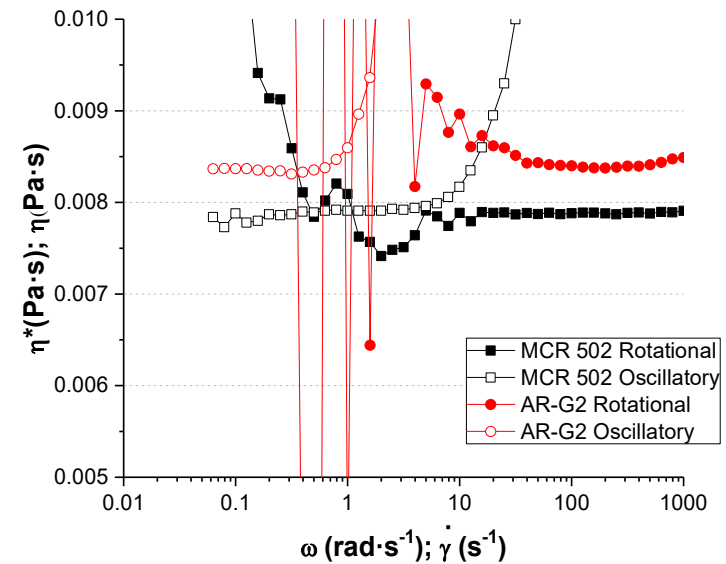


|         | Rotational                      |                       |                                   | Oscillatory                     |                       |                                   |
|---------|---------------------------------|-----------------------|-----------------------------------|---------------------------------|-----------------------|-----------------------------------|
|         | Average viscosity value (mPa·s) | Average deviation (%) | Relative standard uncertainty (%) | Average viscosity value (mPa·s) | Average deviation (%) | Relative standard uncertainty (%) |
| AR-G2   | 3.444                           | 1.29                  | 1.36                              | 3.222                           | -5.23                 | 0.24                              |
| MCR 502 | 3.486                           | 2.53                  | 0.22                              | 3.500                           | 2,94                  | -                                 |
| IMETER  | 3.112                           | -8.47                 | 0.32                              | -                               | -                     | -                                 |

## Rotational mode

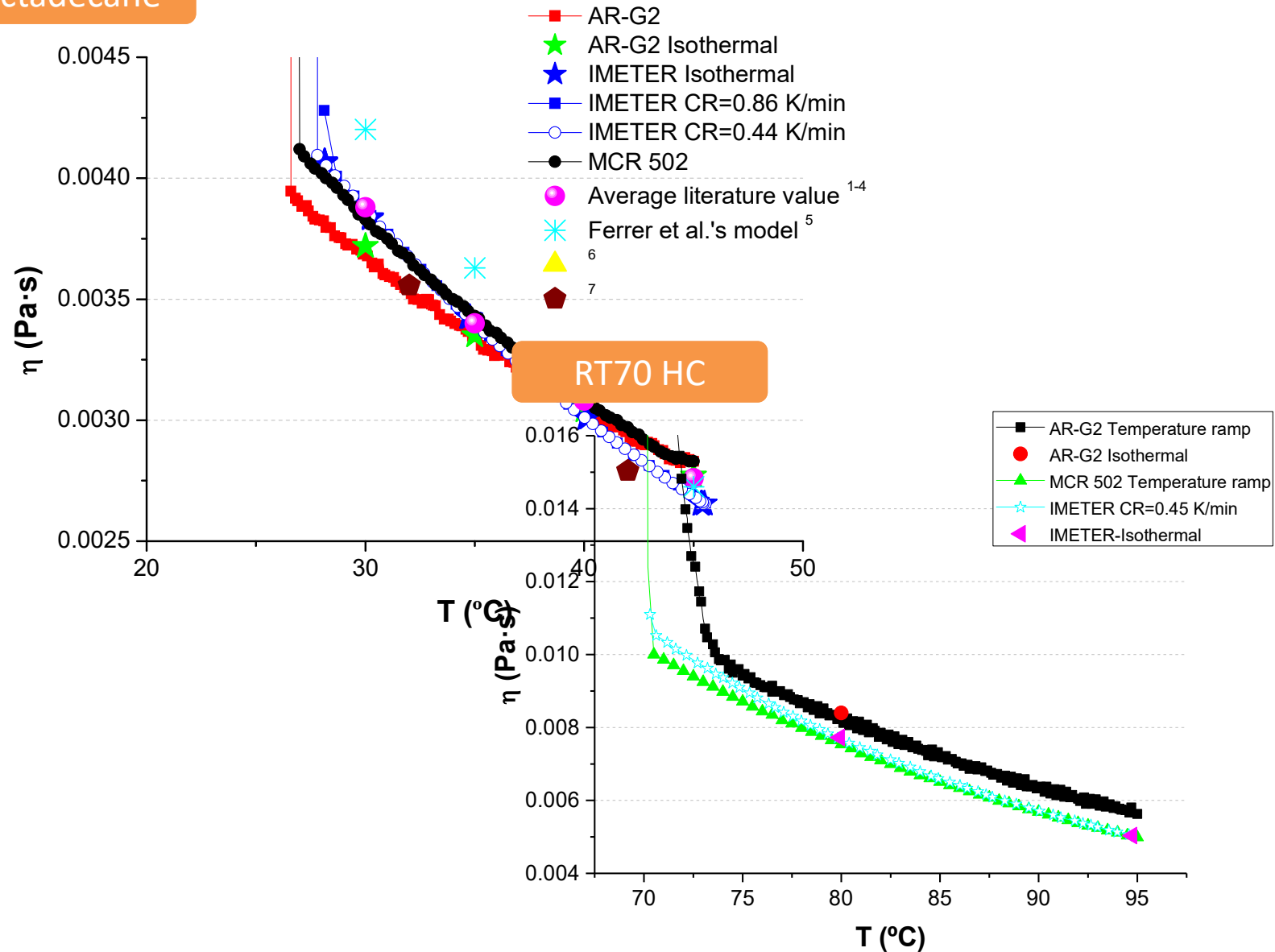


## Oscillatory mode



|         | Rotational                      |                                   | Oscillatory             |                                   |
|---------|---------------------------------|-----------------------------------|-------------------------|-----------------------------------|
|         | Average viscosity value (mPa·s) | Relative standard uncertainty (%) | Average viscosity value | Relative standard uncertainty (%) |
| AR-G2   | 8.388                           | 0.05                              | 8.350                   | 0.09                              |
| MCR 502 | 7.873                           | 0.10                              | 7.880                   | 0.14                              |
| IMETER  | 7.682                           | 0.28                              | -                       | -                                 |

## Octadecane



## 4

# Conclusions



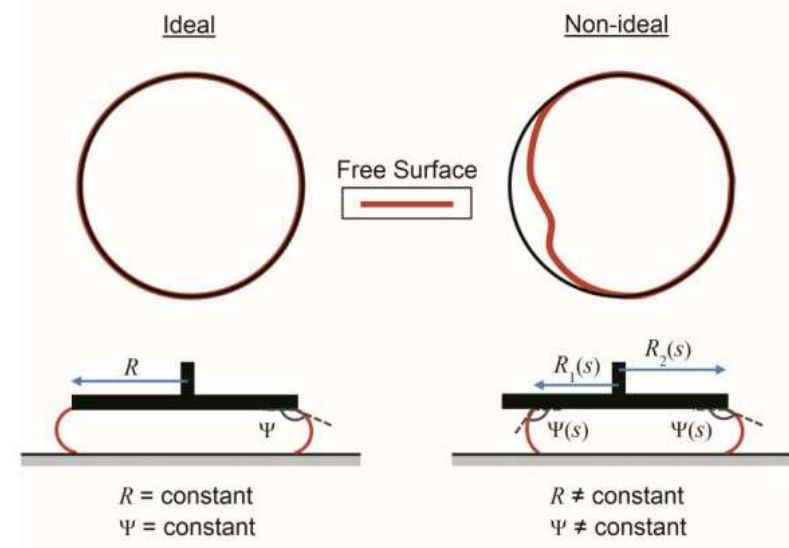
- Good agreement between the viscosities measured with the different rheometer types and between the certified values for standard oil S3 and octadecane.
- Requirement of temperature-controlled geometry or a temperature-controlled hood at elevated temperatures.
- The procedures in both rotational and in oscillatory mode turn out to be appropriate to accurately measure viscosity.
- Experimental window with limitations at high shear rates or frequencies due to instrument and sample inertia, as well as a limitation at low shear rates due to the torque limit.
- Average deviations when measuring S3:
  - Below 7.18 % in rotational mode for the two controlled stress rheometers
  - Below 3.86% in oscillatory mode for the AR-G2 rheometer
  - Below 6.73% in oscillatory mode for the MCR 502 rheometer
  - Below 2.03% for the translational rheometer IMETER

# 5

## Next steps

- First material proposed to be measured →  $\text{KNO}_3$  (molten salt considered as high temperature standard)
- Change of the temperature controller: Peltier plate → Oven
- Main characteristics of the sample and problems encountered:
  - 1) Low viscous fluid
    - Low viscous torque
    - Secondary flows
    - Outward migration
  - 2) High surface tension

- Surface tension results in a torque that should not occur in an ideal, rotationally-symmetric geometry.
- It appears as a constant torque independent of rate  
→ newtonian liquids as shear thinning
- This surface tension torque is sensitive to wetting conditions and contact line asymmetries and cannot be corrected in experimental measurements.



When must be this phenomenon considered?



When low viscous and high surface fluids are being measured

| Substance                      | Surface tension ( $\text{mJ}\cdot\text{m}^{-2}$ ) | Viscosity ( $\text{mPa}\cdot\text{s}$ ) |
|--------------------------------|---------------------------------------------------|-----------------------------------------|
| Water                          | 73 (20°C)                                         | 1.0016 (20°C)                           |
| n-dodecane <sup>9</sup>        | 22 (50°C)                                         |                                         |
| n-octacosane <sup>9</sup>      | 22 (125°C)                                        |                                         |
| KNO <sub>3</sub> <sup>10</sup> | 106 (395°C)                                       | 2.1263 <sup>11</sup> (394°C)            |

How can we face to this problem ?



Measuring at high shear rates

$$\dot{\gamma} = \frac{U}{H}$$

1) Increase the velocity → loss of viscometric flow

2) Reduce the gap → non-parallelism between the plates

At very high shear rates, there are also factors that influence on the rheometric measurements:

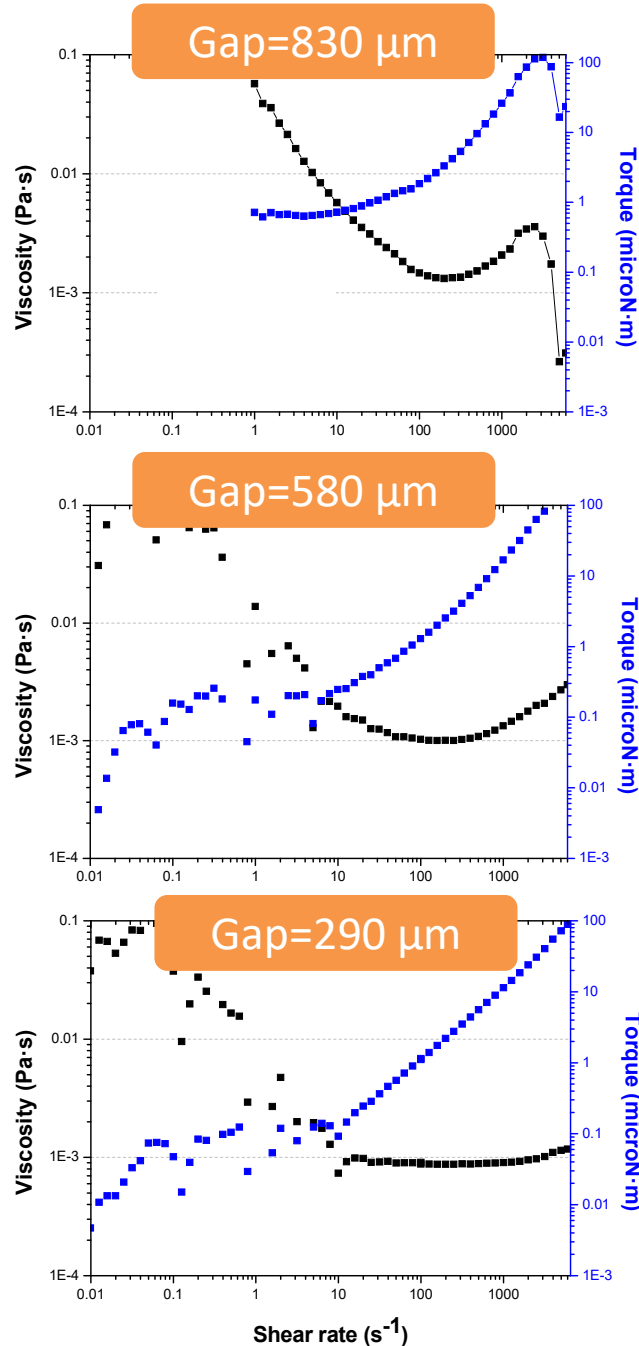
- Inertial effects → secondary flows  
Secondary flows increase the measured torque.

$$\frac{T}{T_0} = 1 + \frac{3}{4900} \cdot Re^2$$

- Radial migration effect → when centrifugal stresses overcome surface tension stresses and the confined fluid is partially ejected → drop in measured torque → drop in measured viscosity

$$\dot{\gamma}_c = \sqrt{\frac{20 \cdot \sigma}{3 \cdot \rho \cdot H}}$$

- Viscous heating



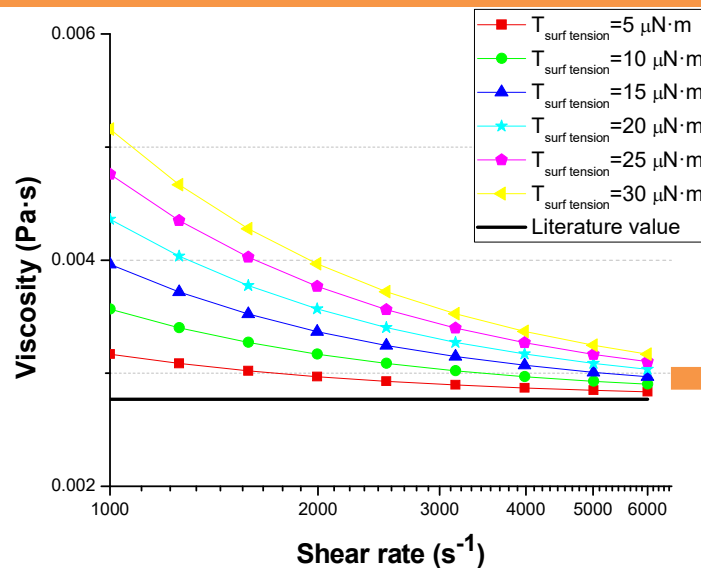
- Constant torque around  $0.7 \mu\text{N}\cdot\text{m}$
- Secondary flows from approx.  $100 \text{ s}^{-1}$
- Outward migration from approx.  $2000 \text{ s}^{-1}$
- A newtonian plateau is not observed

- Constant torque around  $0.2 \mu\text{N}\cdot\text{m}$
- Outward migration is avoided
- Secondary flows from approx.  $500 \text{ s}^{-1}$
- Average viscosity= $1.030 \text{ mPa}\cdot\text{s}$   
Shear rate range [ $50\text{-}400 \text{ s}^{-1}$ ]  
Deviation= $15\%$

- Constant torque around  $0.12 \mu\text{N}\cdot\text{m}$
- Secondary flows is hardly observed
- Wider newtonian plateau observed
- Average viscosity= $0.891 \text{ mPa}\cdot\text{s}$   
Shear rate range [ $25\text{-}1000 \text{ s}^{-1}$ ]  
Deviation= $0\%$

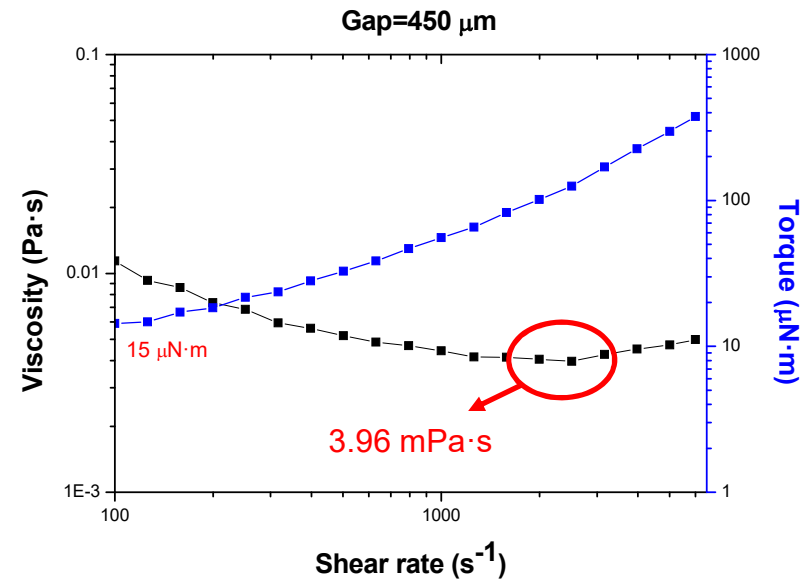
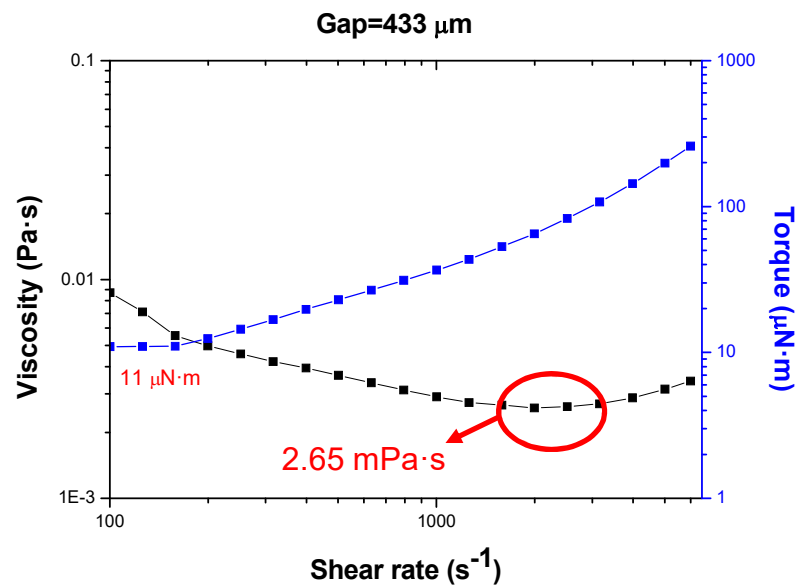
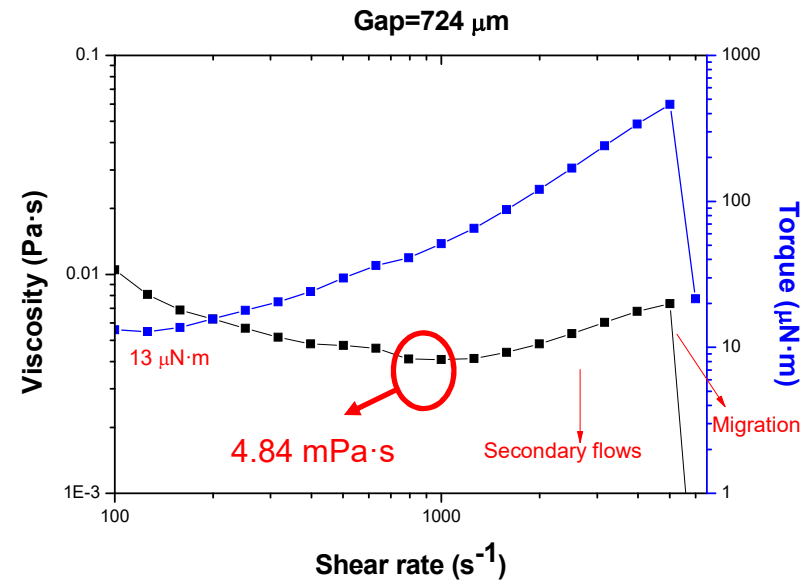
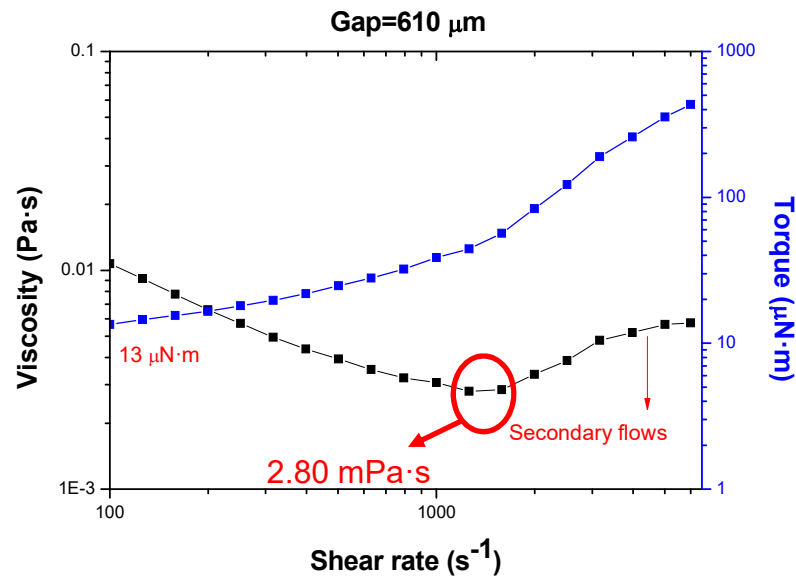
- Samples of  $\text{KNO}_3$  with different gaps have been tested. Gap range [309-890  $\mu\text{m}$ ]
- Constant torque independent of the shear rate within the range [9-26  $\mu\text{N}\cdot\text{m}$ ], which depends on how well the sample has been loaded (in terms of rotational symmetry), as consequence of the surface tension.
- We should pay the attention to the measurements with low gaps to avoid secondary flows and outward migration and with low constant torque due to surface tension.

Theoretical calculation of the influence of the torque due to surface tension on the  $\text{KNO}_3$  viscosity



Surface tension torque should be lower than 15  $\mu\text{N}\cdot\text{m}$  for deviations lower than 10%

$$\eta_{\text{KNO}_3} = 2.77 \text{ mPa}\cdot\text{s}$$



Thank you!  
Any question?